

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE
REQUEST FOR FILING NATIONAL PATENT APPLICATION

Under 35 USC 111(a) and Rule 53(b)

PATENT APPLICATION

WITH SIGNED DECLARATION

NONPROVISIONAL
NON REISSUE
NON PCT NAT PHASE

Commissioner of Patents
Washington, D.C. 20231

Sir:

Herewith is the PATENT APPLICATION of
Inventor(s): SHIRAI et al.

Title THIN INJECTION MOLDED ARTICLES

Atty. Dkt.: PM 275275 ND-TCK-H224-US
M# Client Ref

including:

Date: November 2, 2000

1. Specification: 13 pages (only spec. and claims) 2. ☐ Specification in non-English language
3. Declaration ☒ Original ☐ Facsimile/Copy ☒ Abstract 1 page(s); 3 numbered claims
4. ☒ Drawings: 9 sheet(s) ☐ informal; ☒ formal of size: ☒ A4 ☐ 11"
5. ☐ See top first page re prior Provisional, National or International application(s). ("X" box only if info is there and do not complete corresponding item 5 or 6). (Prior M# SN)
6. **AMEND the specification** please by inserting before the first line: -- This is a ☐ Continuation-in-Part
☐ Divisional ☐ Continuation ☐ Substitute Application (MPEP 201.09) of:
6(a) ☐ National Appln. No. / filed (M#)
6(b) ☐ International Appln. No. filed
7. ☐ **AMEND the specification** by inserting before the first line: -- This application claims the benefit of U.S.
Provisional Application No. 60/ , filed
8. ☒ Attached is an assignment and cover sheet. Please return the recorded assignment to the undersigned.
9. ☐ Prior application is assigned to

by Assignment recorded Reel Frame

10. **FOREIGN** priority is claimed under 35 USC 119(a)-(d)/365(b) based on filing in Japan
11. (country)

Application No.	Filing Date	Application No.	Filing Date
(1) 11-321414	November 11, 1999	(2)	
(3)		(4)	
(5)		(6)	
(7)		(8)	
(9)		<input type="checkbox"/> See 3 rd page for additional priorities	

12. (No.) Certified copy (copies): ☐ attached; ☐ previously filed (date) in U.S. Application No. / filed on
13. Small entity status ☐ is not claimed; ☐ is claimed (Pre-filing confirmation required)
13(a). ☐ Attached: (No.) Small Entity Statement(s) (since 9/8/00 small entity statement(s) not essential to make claim)

14. DOMESTIC/INTERNATIONAL priority is claimed under 35 USC 119(e)/120/365(c) based on the following provisional, nonprovisional and/or PCT international application(s):

Application No.	Filing Date	Application No.	Filing Date
(1)		(4)	
(2)		(5)	
(3)		(6)	

15. ☐ This application is being filed under Rule 53(b)(2) since an inventor is named in the enclosed Declaration who was not named in the prior application.

16. ☐ Attached:

17. ☒ Preliminary Amendment: attached

THE FOLLOWING FILING FEE IS BASED ON CLAIMS AS FILED LESS ANY ABOVE CANCELLED

				Large/Small Entity		Fee Code
18. Basic Filing Fee				\$710/\$355	\$710	101/201
19. Total Effective Claims	4	minus 20 =	*0	x \$18/\$9 =	+ 0	103/203
20. Independent Claims	1	minus 3 =	*0	x \$80/\$40 =	+ 0	102/202
*If answer is zero or less, enter "0"						
21. If any proper multiple dependent claim (ignore improper) is present, add (Leave this line blank if this is a reissue application)				+ \$270/\$135	+ 0	104/204
22. TOTAL FILING FEE ENCLOSED =					\$710	
23. If "non-English" box 2 is X'd, add Rule 17(k) processing fee				+ \$130	+ 0	139
24. If "assignment" box 8 is X'd, add recording fee				+ \$40	+ 40	581
25. <input type="checkbox"/> Attached is a Petition/Fee under Rule No.				+ \$130	+ 0	122
26. TOTAL FEE ENCLOSED =					\$750	

Our Deposit Account No. 03-3975

Our Order No. 11349 C# 275275 M#

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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re PATENT APPLICATION OF

SHIRAI et al.

Application No.: New Application

Group Art Unit: Unknown

Filed: November 2, 2000

Examiner: Unknown

FOR: THIN INJECTION MOLDED ARTICLES

* * * * *

November 2, 2000

PRELIMINARY AMENDMENT

Hon. Commissioner of Patents
and Trademarks
Washington, D.C. 20231

Sir:

Please enter the following amendments and consider the following remarks prior to examination.

IN THE CLAIMS

Claim 3, line 1, delete "or 2"

Please add new claim 4.

--4. A molded article according to claim 2, wherein said organic clay is clay that has been rendered organic with two or more different types of organic agents.--

APPLICATION UNDER UNITED STATES PATENT LAWS

Atty. Dkt. No. PM 275275
(M#)

Invention: THIN INJECTION MOLDED ARTICLES

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This is a:

- ☐ Provisional Application
- ☒ Regular Utility Application
- ☐ Continuing Application
 - ☒ The contents of the parent are incorporated by reference
- ☐ PCT National Phase Application
- ☐ Design Application
- ☐ Reissue Application
- ☐ Plant Application
- ☐ Substitute Specification
 - Sub. Spec Filed _____
 - in App. No. _____ / _____
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 - Sub. Spec. filed _____
 - In App. No _____ / _____

SPECIFICATION

THIN INJECTION MOLDED ARTICLES

BACKGROUND OF THE INVENTION

5 1. Field of the Invention

The present invention relates to thin injection molded articles which are lightweight and have a required rigidity.

10 2. Description of the Related Art

Attempts to create thinner injection molded parts usually result in a lack of rigidity. The resins used in such thin parts must therefore satisfy the reciprocal properties of, firstly, high rigidity of thin sections, and secondly, high flow properties of the resin during injection.

Rigidity has conventionally been improved by adding glass fiber to resins.

However, when glass fiber is added to a resin, the flow properties during resin melting are reduced, thus impairing the molding properties of the thin part. When injection molding is forcibly carried out under severe molding conditions such as high speed and high pressure in order to improve the molding property, there is a risk of deterioration of the resin by shear heat between the resin and the mold.

Thin resin parts must also be lightweight and have good electrical insulating properties.

It has also been proposed to add organic clay to polymers instead of glass fiber (Japanese Unexamined Patent Publication HEI No. 11-92677).

BRIEF SUMMARY OF THE INVENTION

In light of these problems of the prior art, it is an object of the present invention to provide lightweight thin injection molded articles with high rigidity and excellent electrical insulating properties.

The present invention provides a thin injection molded article composed of a composite resin material

having organic clay dispersed in a polymer,
wherein the polymer comprises polyphenylene
oxide and a butadiene-styrene copolymer, and
the relationship between the maximum flow
length L of the composite resin material in the thin
injection molded article and the average thickness t of
the thin injection molded article satisfies the
inequality: $L/t \geq 70$.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is an illustration showing the relationship
between polyphenylene oxide (PPO) and clay rendered
organic with one type of organic agent.

Fig. 2 is an illustration showing the relationship
between PPO and clay rendered organic with two or more
types of organic agent.

Fig. 3 is an illustration showing organic clay and a
polymer according to the invention.

Figs. 4a, 4b, 4c and 4d are perspective views of
cavities for injection molding, for illustration of
different gate shapes and maximum flow lengths according
to the invention.

Figs. 5a and 5b are perspective views of thin
injection molded articles.

Figs. 6a, 6b, 6c, 6d, 6e and 6f are illustrations
showing the flow condition of a resin in a cavity for
examples and comparative examples.

Fig. 7 is a line graph showing the relationship
between tensile modulus and L/t for thin injection molded
articles of the examples and the comparative examples.

Fig. 8 is a line graph showing the relationship
between filler content and relative tensile modulus for
thin injection molded articles of the examples and the
comparative examples.

Fig. 9 is a line graph showing the relationship
between maximum flow length L and L/t for thin injection
molded articles with the rigidity required for
manufactured products, according to the examples and the

comparative examples.

DETAILED DESCRIPTION OF THE INVENTION

Polymers made of polyphenylene oxide (hereunder, "PPO") and butadiene-styrene copolymer (hereunder, "BS copolymer") have high compatibility with organic clay. Composite resins composed of such polymers and organic clay can guarantee high rigidity for injection molded articles, and thus allow realization of thinner injection molded articles. The injection molded articles also have lighter specific densities and excellent electrical insulating properties.

Such thin injection molded articles have a relationship between maximum flow length L of the composite resin material and average thickness t of the thin injection molded article that satisfies the inequality $L/t \geq 70$. They consequently have high flow properties and can give thinner injection molded articles. However, when $L/t < 70$ it is no longer possible to achieve thinner injection molded articles.

The present invention, therefore, can provide lightweight thin injection molded articles with high rigidity and excellent electrical insulating properties.

Polymers composed of PPO and BS copolymer include modified polyphenylene oxide (hereunder, "modified PPO"). Modified PPO is a resin of PPO modified with HIPS (high impact polystyrene). Here, the term "modified" means that the PPO and HIPS are kneaded in a molten state. HIPS is a butadiene-styrene block copolymer.

Polymers comprising PPO and BS copolymer have better properties such as clay dispersability, resin flow properties and toughness compared to polymers composed only of PPO and containing no BS copolymer. Modified PPO exhibits an even higher dielectric breakdown.

Organic clay is clay (clay mineral) that has been rendered organic with an organic agent.

As clays there may be mentioned montmorillonite, saponite, hectorite, beidellite, stevensite, nontronite,

vermiculite, halloysite, mica, fluorinated mica, kaolinite, pyroferite, and the like. Natural or synthetic clays may be used. Sheet silicates such as montmorillonite are preferred because they allow greater improvement in mechanical strength.

An example of an organic agent is an organic onium ion.

As organic onium ions there may be used primary to quaternary ammonium ions, such as hexylammonium ion, octylammonium ion, 2-ethylhexylammonium ion, decylammonium ion, dodecylammonium ion, laurylammonium ion, hexadecylammonium ion, octadecylammonium ion, dioctyldimethylammonium ion, trioctylammonium ion, dioctadecyldimethylammonium ion, trioctadecylammonium ion, and the like.

Other organic onium ions include phosphonium ions. As phosphonium ions there may be used tetraethylphosphonium ion, triethylbenzylphosphonium ion, tetra-n-butylphosphonium ion, tri-n-butylhexadecylphosphonium ion, tri-n-butylbenzylphosphonium ion, and the like.

The organic clay content in the thin injection molded article of the invention is preferably 1-5 parts by weight to 100 parts by weight of the polymer. With less than 1 part by weight there is a risk of insufficient rigidity of the molded article. With greater than 15 parts by weight, the molded article may become brittle and tend to break.

More preferably, the organic clay content is 3-7 parts by weight to 100 parts by weight of the polymer. This will further improve the rigidity and impact fracture resistance of the molded article.

The organic clay in the molded article of the invention is preferably one wherein the clay has been rendered organic with two or more organic agents. Using such an organic clay can result in a larger L/t ratio, and molding of a thinner injection molded article.

The two or more organic agents may be selected from among the aforementioned primary to quaternary ammonium ions or phosphonium ions. A preferred example is a combination of dodecylammonium ion and octadecylammonium ion, with a dodecylammonium ion/octadecylammonium ion proportion of 0.01-100. The two or more different organic agents and their mixing proportions may be freely selected.

Using an organic clay that has been rendered organic with two or more organic agents can give an even larger L/t ratio and allow molding of thinner molded articles for the reason described below.

As shown in Fig. 1, the clay 11 in the organic clay 1 is surrounded by the organic agent 12. The surface of an organic clay 1 that has been obtained by treatment of clay 11 with one type of organic agent 12 is covered with equal length carbon chains of the organic agent 12, and thus becomes even. On the other hand, as shown in Fig. 2, an organic clay 1 obtained by treatment of clay 11 with two or more different organic agents 12 has an uneven surface due to the different lengths and three-dimensional structures of the organic agents 121, 122. The PPO (20) in the polymer is bonded to the clay 11 by hydrogen bonds or Van der Waals forces, while also interacting and bonding with the organic agent 12 on the surface of the clay 11 or the carbon chains bonded to the organic agent 12. Because blends comprising PPO and BS copolymer are rigid, the interaction occurs more readily with organic clay having a surface covered with even carbon chains. Clay that has been rendered organic with two or more organic agents has an uneven surface, and therefore variation is produced in the interactive force with the PPO, in some cases resulting in sections which undergo no interaction. Thus, when clay has been rendered organic with two or more organic agents such that variation exists in the interactive force, peeling of the organic clay and the PPO tends to occur due to a

shear force produced during injection molding. The flow properties of the composite resin comprising the polymer and organic clay are therefore further improved, allowing molding of a thinner molded article than by using one type of onium ion.

The same effect can also be achieved by using two or more clays rendered organic with organic agents, for molding of thin molded articles. This is for the same reason explained above, as the combination of two or more clays produces variation in the interactive force with the PPO, thus facilitating peeling of the organic clay and PPO.

The organic clay 1 is dispersed in the polymer 2 as shown in Fig. 3.

The organic clay preferably loses its layer structure in the polymer 2, becoming dispersed as a monolayer. This increases the proportion of the polymer restricted by the organic clay, and enhances the reinforcing effect of the organic clay.

The dielectric breakdown is higher when the clay is dispersed as a monolayer. This is because clay is insulating, and the breakdown current cannot pass through and must detour. That is, it appears as if the thickness has been increased.

The organic clay is preferably dispersed to a size of no greater than 1 μm in the polymer. This will improve the mechanical properties of the molded article. The polymer also preferably intervenes between the clay layers. This will increase the interface between the clay surface and the polymer, and enhance the polymer reinforcing effect of the clay.

The distance between the organic clay layers, due to the PPO intervening between the dispersed and separated clay layers, is preferably 50 angstroms or greater. This will enhance the reinforcing effect of the clay on the elastic modulus, etc. The distance between the dispersed and separated organic clay layers is more preferably 100

angstroms or greater. This will exhibit the maximum reinforcing effect.

The layers of the organic clay are preferably separated as described above, but there is no need for all of the clay layers to be separated. There will be variations in the organic treatment of the clay, and portions of the clay may be aggregated. It is sufficient if only a portion adequately exhibits the reinforcing effect.

According to the invention, the relationship between the maximum flow length L of the composite resin material in the thin injection molded article and the average thickness t of the thin injection molded article is such that $L/t \geq 70$. The "maximum flow length of the composite resin material in the thin injection molded article" is the distance between the origin A of the injection molding gate and the furthest point B from the origin A in the thin injection molded article molded in the cavity. The origin A is the site of the gate that is at closest proximity to point B .

For example, as shown in Fig. 4a, in the cavity 4 of a cylinder for molding of a cylindrical thin injection molded article, the maximum flow length L is the distance between the origin A of the gate 41 and the furthest point B at the edge of the cylinder. When multiple gates 41 are provided in the cavity 4, as shown in Fig. 4b, the maximum flow length L according to the invention is the longest flow length of the maximum flow lengths L' , L'' from origins A' , A'' of each gate 41. When the maximum flow lengths L' and L'' from the origins A' , A'' of two gates 41 are equal, as shown in Fig. 4b, either one constitutes the maximum flow length L for the composite resin material of the thin injection molded article.

The "gate" is a narrow opening at the section of the cavity where the molten composite resin material enters from a runner.

The gate 41 may be a pin gate with a point opening

(Fig. 4a, 4b), a film gate with a linear opening (Fig. 4c) or a ring gate with a disk-shaped opening (Fig. 4d). For all of these gates, the maximum flow length L is determined by defining the origin A as the location of the gate nearest the furthest point B .

In the gate 41, a sprue 43 through which the molten composite resin material is supplied is connected via a runner 42 which conducts the composite resin material from the sprue 43 to the gate 41.

According to the invention, the "average thickness t of the thin injection molded article" is the average value for the thickness of the thin injection molded article.

The average thickness t of the thin injection molded article is preferably 0.3-2.0 mm. At less than 0.3 mm the rigidity of the injection molded article may be unsustainable, and at greater than 2.0 mm the weight of the injection molded article may be insufficient.

The shape of the thin injection molded article is not particularly limited so long as it is thin and, for example, it may be planar (Fig. 5a), cylindrical (Fig. 5b), film-like, curved or bent.

The thin injection molded article of the invention may be used as a case housing for an ignition coil bobbin, a cellular phone or the like, but there is no limitation to these uses.

Embodiments of thin injection molded articles of the invention will now be explained with reference to Examples 1-6 and Comparative Examples 1-6

Examples 1-4, Comparative Examples 1-6

First, composite resin materials having the composition listed in Table 1 were prepared. The polymers were modified PPO, PBT (polybutylene terephthalate), PPS (polyphenylene sulfide) and nylon 66.

Composite resin materials comprising modified PPO and organic clay were used for Examples 1-4. A resin material composed only of modified PPO was used for

Comparative Example 1. The organic clay used was montmorillonite rendered organic with stearylammmonium. Composite resin materials with glass fiber added instead of organic clay were used for Comparative Examples 2 and 3. Resin materials composed only of PBT, PPS and NY66 were used for Comparative Examples 4, 5 and 6, respectively.

As shown in Figs. 6a, 6b, 6c, 6d, 6e and 6f, the (composite) resin materials were injection molded from the gate 41 into the cavity 4 through the sprue 43 and runner 42. The cavity 4 has the same shape as the outer surface of the molded article, in order to mold a cylindrical thin molded article. A core 40 with the same shape as the inner surface of the molded article is fitted inside the cavity 4. The thickness of the cavity was 0.7 mm.

As shown in Fig. 5b, the resulting thin injection molded article 3 was a cylinder with an average thickness t of 0.7 mm and having a hollow section 30 at the center.

Example 5

As the organic clay there was used montmorillonite that had been rendered organic with stearylammmonium and dodecylammmonium. The stearylammmonium and dodecylammmonium were mixed in a ratio of stearylammmonium/dodecylammmonium = 0.8/0.2 (weight ratio) for treatment of the montmorillonite. The other conditions were the same as in Example 2 for preparation of the composite resin material.

Example 6

As the organic clay there was used montmorillonite that had been rendered organic with stearylammmonium and hexadecylammmonium. The stearylammmonium and hexadecylammmonium were mixed in a ratio of stearylammmonium/hexadecylammmonium = 0.5/0.5 (weight ratio) for treatment of the montmorillonite. The other conditions were the same as in Example 3 for preparation of the composite resin material.

The spiral flow length, maximum flow length/average thickness (L/t), thin injection molded article tensile modulus and dielectric breakdown strength of the (composite) resin material of the thin injection molded article were measured, and the results are shown in Table 1. The spiral flow length is the value measured by a common resin flow property test. The maximum flow length of the thin injection molded article is the distance between the origin A of the gate shown in Fig. 4c and the furthest point B at the edge of the cylinder.

The same table shows that Examples 1-6 of the invention had large L/t ratios and high values for tensile modulus and dielectric breakdown strength. The L/t ratios were large in Examples 5 and 6. This demonstrates that, when using clay that has been rendered organic with two types of organic agents, the flow properties of the composite resin are even higher, and even better molding properties and increased thinness can be achieved.

In contrast, in Comparative Example 1 that was composed only of modified PPO, the L/t ratio was large but the tensile modulus and dielectric breakdown strength were low. The dielectric breakdown strength for Comparative Examples 4-6 that were composed of polymers other than modified PPO were even lower than Comparative Example 1 that was composed only of modified PPO.

Also, since the composite resins wherein glass fiber was added to the modified PPO (Comparative Examples 2 and 3) had high glass fiber contents of 10 parts by weight and 20 parts by weight respectively, their L/t ratios were smaller than that of the composite resins wherein organic clay was added to the modified PPO (Examples 1-4).

Examples 2 and 3 also had higher dielectric breakdown strengths than Comparative Examples 1, 2 and 3, since the dielectric breakdown strengths were enhanced due to the clay.

Table 1

	Comp. Ex. 1	Example 1	Example 2	Example 3	Example 4	Example 5	Example 6	Comp. Ex. 2	Comp. Ex. 3	Comp. Ex. 4	Comp. Ex. 5	Comp. Ex. 6
Modified PPO	100	100	100	100	100	100	100	100	100	100		
PBT										100		
PPS											100	
NY66												100
Organic clay (*)		1 (1)	3 (1)	5 (1)	7 (1)	3 (2)	5 (2)					
Glass fiber								10	20			
Spiral flow length (mm)	57.2	55.4	54.5	53.3	52.7	54.7	53.8	50.6	48.3			
Max flow length/average thickness (L/t)	105	94	88	81	78	93	88	64	50			
Tensile modulus (GPa)	2.40	2.59	2.93	3.24	3.62	3.33	3.35	3.33	4.72			
Dielectric breakdown strength (kv/mm)	21.1		21.9	22.7				21.0	20.3	17	18	16

(*) Number of organic agent types

Fig. 7 shows the relationship between tensile modulus and maximum flow length for Examples 1-6 and Comparative Examples 1-3. As seen here, the composite materials of modified PPO and organic clay (Examples 1-4) were able to provide higher rigidity for the molded articles with the same maximum flow length, compared to the composite materials of modified PPO and glass fiber.

The experimental results for Examples 5 and 6 also demonstrated that the maximum flow length can be increased by using clay rendered organic with two types of organic agents.

Fig. 8 shows the relationship between the content of the filler (organic clay or glass fiber) in Examples 1-6 and Comparative Examples 1 and 2, and the tensile modulus of the molded product. In Fig. 8, the horizontal axis represents the filler content with respect to 100 parts by weight of polymer, and the vertical axis represents the relative tensile modulus with the tensile modulus of Comparative Example 1 defined as 1.

According to this graph, the rigidity of the composite material comprising modified PPO and organic clay reflected twice the reinforcing effect with the same filler content, compared to the composite resin material comprising modified PPO and glass fiber.

As shown in Fig. 9, measurement of the L/t ratio satisfying the rigidity required for manufactured products (3-5 GPa) indicated that the composite resin materials comprising organic clay and modified PPO had larger L/t ratios than the composite resin materials comprising glass fiber and modified PPO. Thus, by using a composite resin material having organic clay dispersed in modified PPO, it is possible to produce thin, lightweight injection molded articles with excellent rigidity.

We claim:

1. A thin injection molded article composed of a composite resin material having organic clay dispersed in a polymer,

5 wherein said polymer comprises polyphenylene oxide and a butadiene-styrene copolymer, and

10 the relationship between the maximum flow length L of said composite resin material in said thin injection molded article and the average thickness t of the thin injection molded article satisfies the inequality: $L/t \geq 70$.

15 2. A molded article according to claim 1, wherein the content of said organic clay is 1-15 parts by weight to 100 parts by weight of the polymer.

3. A molded article according to claim 1 or 2, wherein said organic clay is clay that has been rendered organic with two or more different types of organic agents.

THIN INJECTION MOLDED ARTICLES

5

ABSTRACT OF THE DISCLOSURE

10 A thin injection molded article is composed of a
composite resin material of organic clay 2 dispersed in a
polymer 1. The polymer comprises a blend of
polyphenylene oxide and a butadiene-styrene copolymer.
The relationship between the maximum flow length L of the
composite resin material in the thin injection molded
article and the average thickness t of the thin injection
15 molded article satisfies the inequality: $L/t \geq 70$.

Fig.1

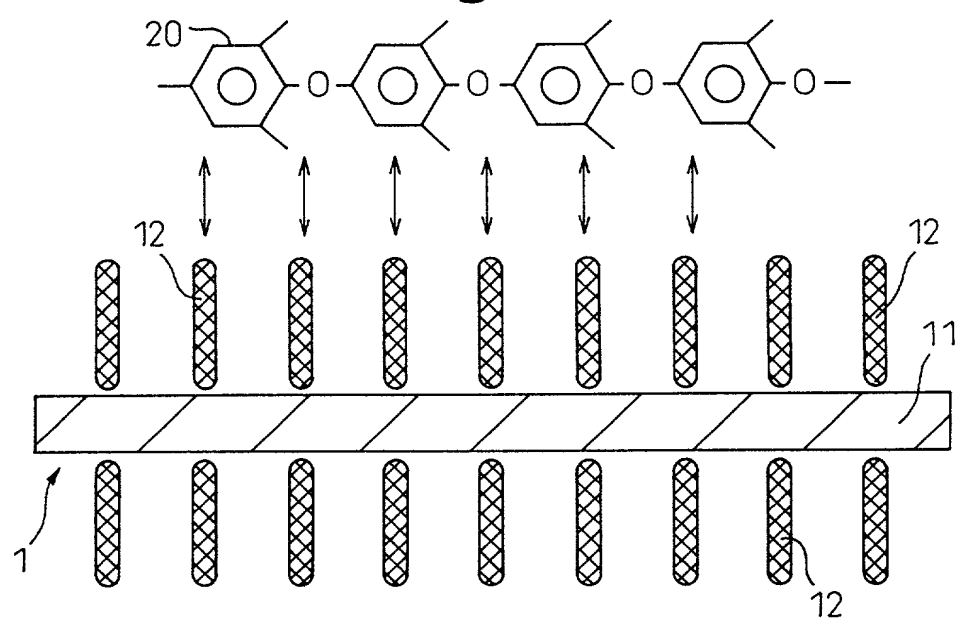


Fig.2

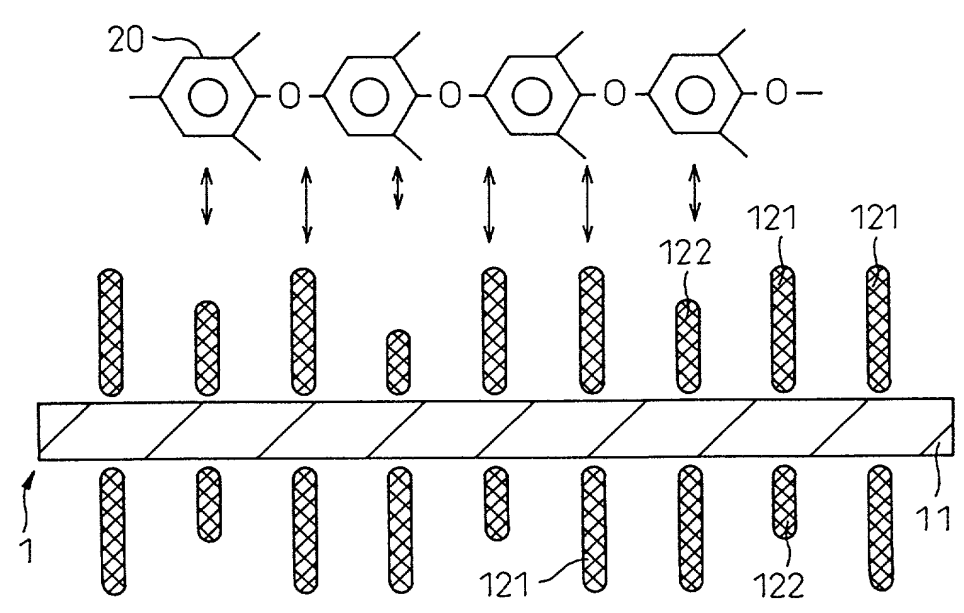


Fig.3

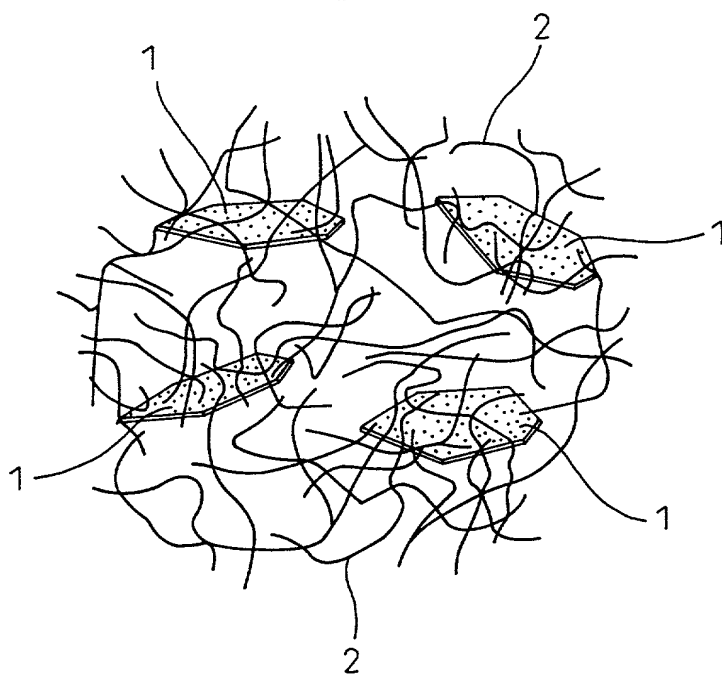


Fig.4a

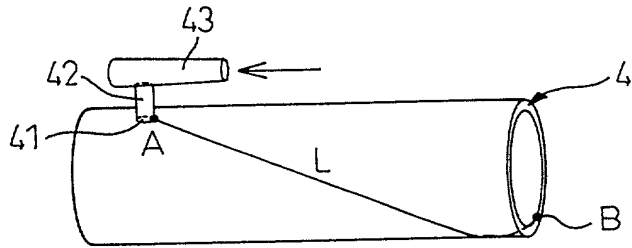


Fig.4b

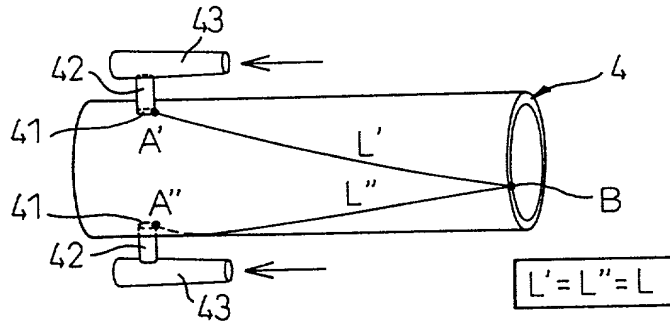


Fig.4c

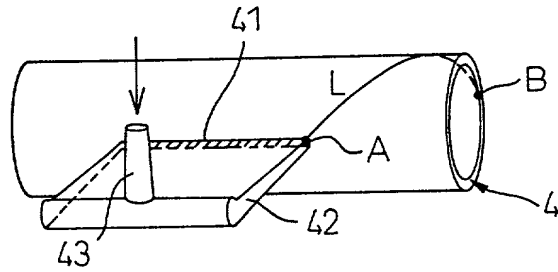


Fig.4d

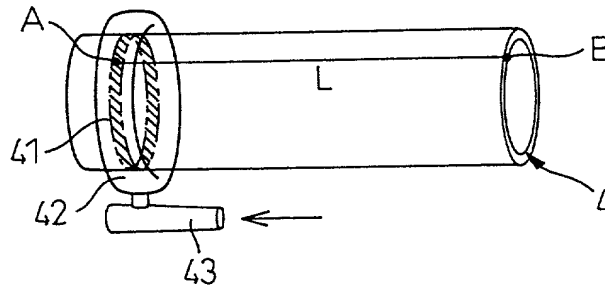


Fig.5a

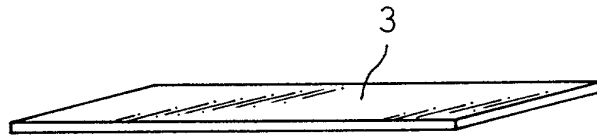


Fig.5b

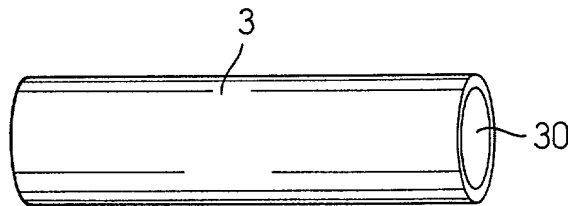


Fig.6a

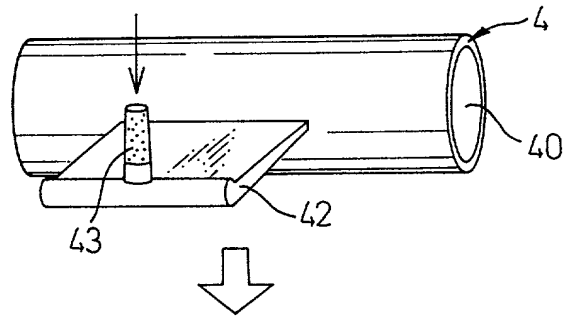


Fig.6b

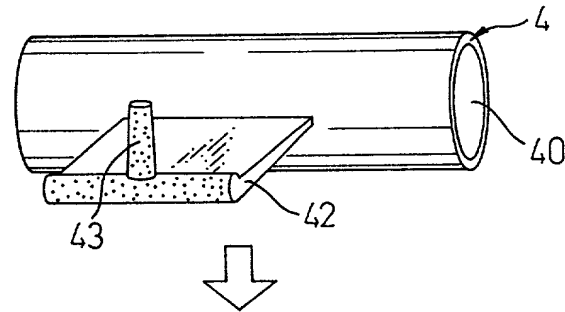
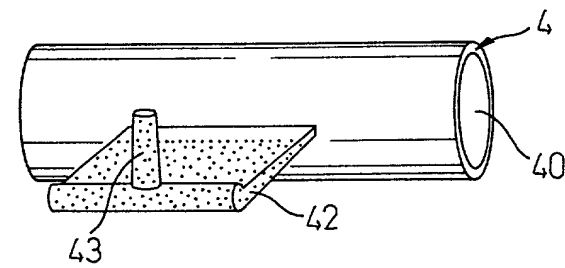


Fig.6c



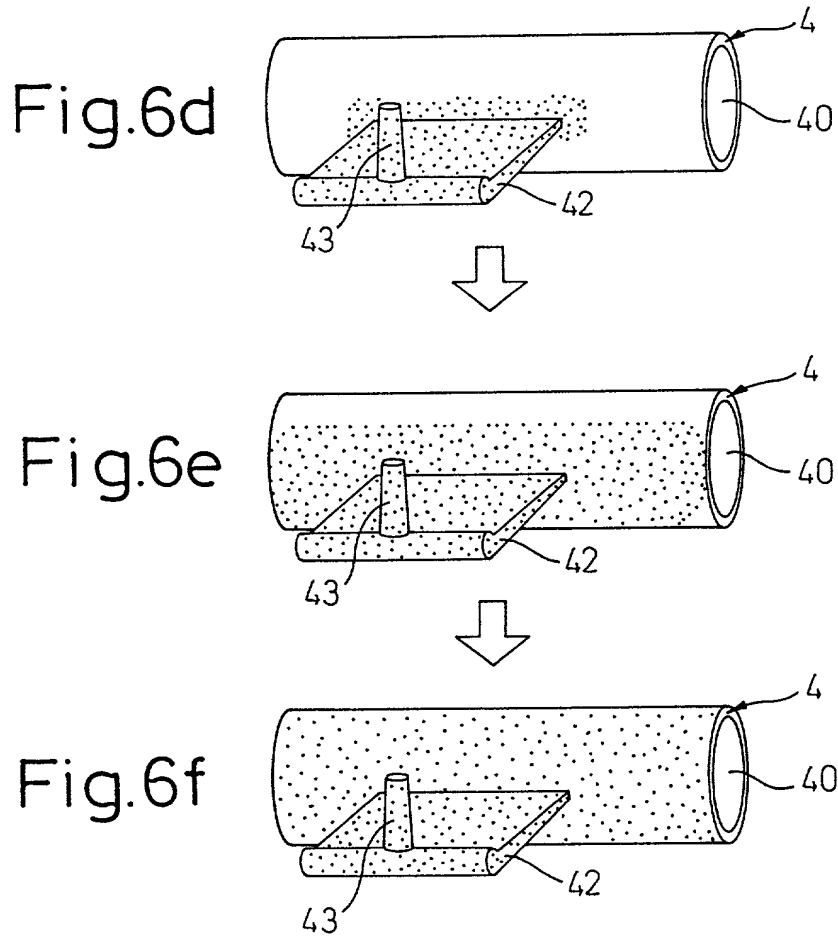


Fig.7

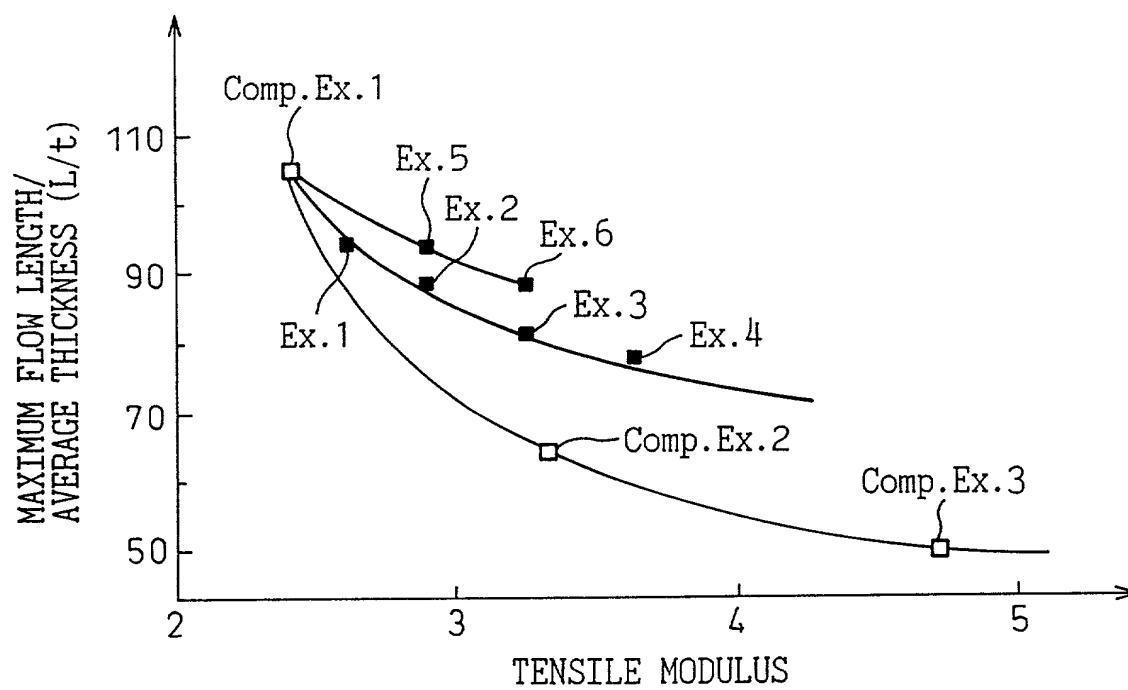


Fig.8

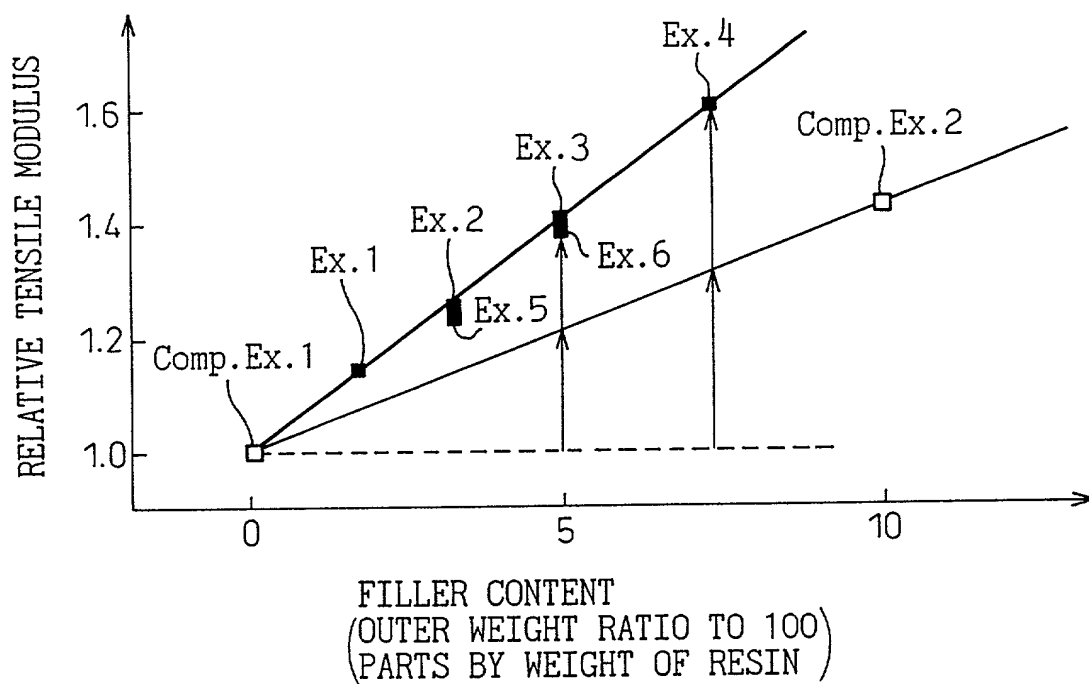
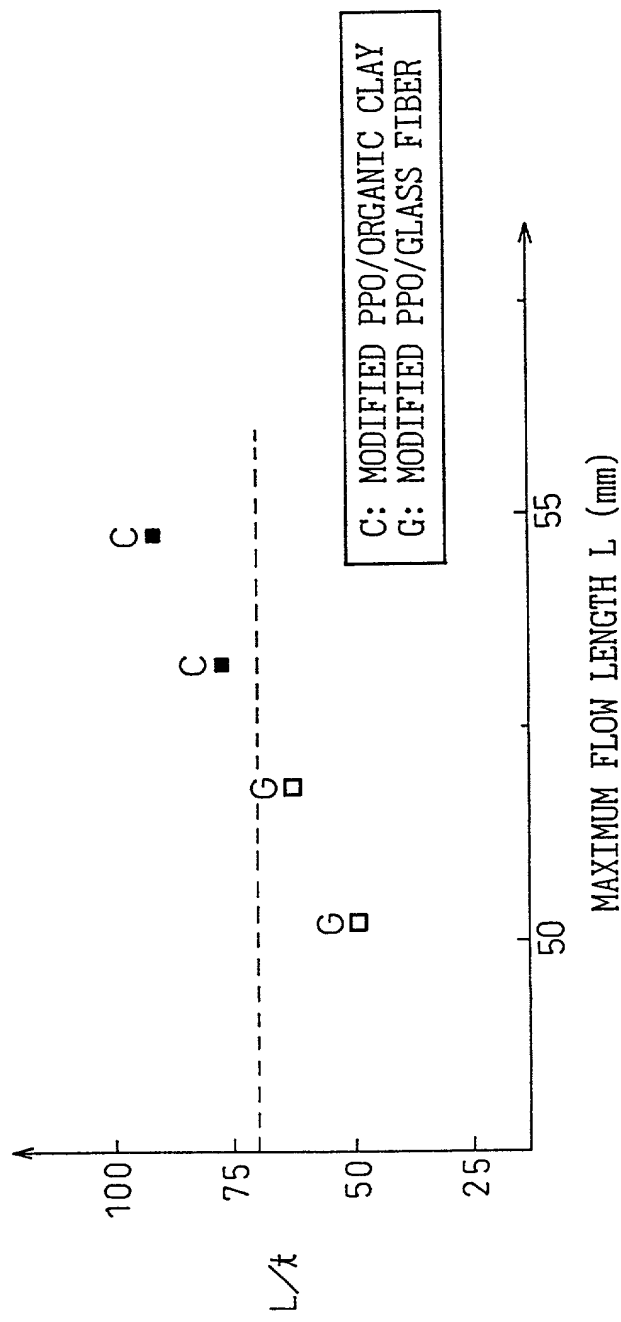


Fig.9



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Declaration and Power of Attorney For Patent Application

特許出願宣言書及び委任状

Japanese Language Declaration

日本語宣言書

下記の氏名の発明者として、私は以下の通り宣言します。

As a below named inventor, I hereby declare that:

私の住所、私書箱、国籍は下記の私の氏名の後に記載された通りです。

My residence, post office address and citizenship are as stated next to my name.

下記の名称の発明に関して請求範囲に記載され、特許出願している発明内容について、私が最初かつ唯一の発明者（下記の氏名が一つの場合）もしくは最初かつ共同発明者であると（下記の名称が複数の場合）信じています。

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

THIN INJECTION MOLDED ARTICLES

上記発明の明細書（下記の欄でx印がついていない場合は、本書に添付）は、

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 （該当する場合）____に訂正されました。

☐ was filed on _____
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Prior Foreign Application(s)

外国での先行出願

11-321414 (Pat.Appln.)

Japan

(Number)
(番号)

(Country)
(国名)

(Number) -
(番号)

(Country)
(国名)

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(出願番号)

(Filing Date)
(出願日)

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(出願番号)

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Priority Not Claimed

優先権主張なし

11/November/1999

(Day/Month/Year Filed)
(出願年月日)

(Day/Month/Year Filed)
(出願年月日)

I hereby claim the benefit under Title 35, United States Code, Section 119(e) of any United States provisional application(s) listed below.

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(出願番号)

(Filing Date)
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I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s), or 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of application.

(Status: Patented, Pending, Abandoned)
(現況: 特許許可済、係属中、放棄済)

(Status: Patented, Pending, Abandoned)
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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委任状: 私は下記の発明者として、本出願に関する一切の手続きを米特許商標局に対して遂行する弁理士または代理人として、下記の者を指名いたします。(弁理士、または代理人の氏名及び登録番号を明記のこと)

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and transact all business in the Patent and Trademark Office connected therewith (list name and registration number)

And I hereby appoint Pillsbury Madison & Sutro LLP, Intellectual Property Group, 1100 New York Avenue, N.W., Ninth Floor, East Tower, Washington, D.C. 20005-3918, telephone number (202) 861-3000 (to whom all communications are to be directed), and the below-named persons (of the same address) individually and collectively my attorneys to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith and with the resulting patent, and I hereby authorize them to delete names/numbers below of persons no longer with their firm and to act and rely on instructions from and communicate directly with the person/assignee/attorney/firm/ organization who/which first sends/sent this case to them and by whom/which I hereby declare that I have consented after full disclosure to be represented unless/until I instruct the above Firm and/or a below attorney in writing to the contrary.

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Raymond F. Lippitt	17519	George M. Sirilla	18221	Michelle N. Lester	32331	Paul F. McQuade	31542
G. Lloyd Knight	17698	Donald J. Bird	25323			Ruth N. Morduch	31044
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Edgar H. Martin	20534	Peter W. Gowdey	25872	Lynn E. Eccleston	35861	Roger R. Wise	31204
William K. West, Jr.	22057	Dale S. Lazar	28872	David A. Jakopin	32995		
Kevin E. Joyce	20508	Glenn J. Perry	28458	Mark G. Paulson	30793		
		Kendrew H. Colton	30368	Timothy J. Klima	34852		

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seventh and subsequent joint inventors.)